OPTIMAL ALLOCATION OF ENERGY STORAGE SYSTEM (ESS) AND UPQC BY PSO FOR GRID CONNECTED WIND MODEL

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Abstract

In the ambiance of renewable energy integrated grid of electricity generation, the endeavor of energy storage strategy (ESS) has been an inevitable technique to abduct the energy by means of renewable sources and endow during the obligation of huge electrical energy. Inoculation of the wind power into an electric grid affects the power quality. The arbitrary arrangement of ESS in the grid integration has prompt pessimistic characteristic. Vanquishing this bothersome impact of ESS in this errand, one of the meta-heuristic portrayal particle swarm optimization (PSO) has been resolved since requires less computational stretch and depicts in MATPOWER. The proposed model outfits the ideal area of ESS in the system of electricity generation and idealistic aspect of ESS. In this paper introduces a complete audit on the unified power quality conditioner (UPQC) to improve the electric power quality at appropriation levels and also the execution of PSO over the test system relates with pertinence of optimal power flow (OPF) model with assorted investigations, to prognosis the envisage of PSO to forfeiture the unfortunate costs and real power shortfalls imports to transmission for conservative generation of electric power. In this proposed plot UPQC is associated at a state of regular coupling with a battery energy storage system (BESS) to alleviate the power quality issues. The battery energy storage is coordinated to maintain the real power source under fluctuating wind power. The UPQC control conspire for the grid associated wind energy generation system for power quality renovation is simulated using MATLAB/SIMULINK in power system block set.

Keywords: Particle swarm optimization, energy storage system, wind energy conversion system, UPQC.

1. Introduction

To have reasonable development and social advance, it is important to meet the energy require by using the renewable energy resources like wind, biomass, hydro, co-generation, etc. In feasible energy framework, energy conservation and **C.K Babulal** Thiagarajar College of Engineering, Madurai, Tamil Nadu ckbabulal@gmail.com

the utilization of renewable source are the key worldview. At the beginning, coal is the preeminent real asset used to generate the electrical energy nonetheless the need of electrical energy had expanded and after that the researchers investigate distinct resources accessible in the earth initiated to utilize the endowed sources such natural gas and nonconventional energy resources. The worldwide energy commitments by oil, gas, coal and non-fossil fuels each will be around 25% in 2040.Withal renewable energy sources are abrupt expanding and contribute around 14% of prime energy.

It has been consistently a threat to preserve the quality of electric power within the tolerable restraint [1-7]. The need to desegregate the renewable energy like wind energy into power system is to make it conceivable to limit the ecological impact on conventional plant [11]. In this framework of wind energy scheme (WES) and energy storage strategy (ESS) have been converged in the expected IEEE-30 bus test system, nevertheless the due to stochastically nature of wind, excess energy generated has been reserved in energy storage strategy. Ideal rating of the energy storage system with respect to the grid endurance examined in [8&9].

The integration of ESS determined the grid with improved power quality and has the ability to intensify the stability of the power system as apprise in [10]. The particle swarm optimization and its assorted form of algorithm were used for the best arrangement of ESS in the grid as all-inclusive in [12,13,14,15&16].

A new terminology to resolve the power quality index is disused in [17&18]. In [19] the power quality of wind associated grid is investigated utilizing wavelet packet transform. Point scheme strategy is used to examine the harmonics and quality of power as in [20]. The stability of wind turbines after they associated with the grid is resolved in [21]. The wind energy fore- casted by time series and neural network as in [22] and ARMA (autoregressive moving average) and ANN (artificial neural networks) as described in [23]. In recent years, the technological advancement of high power electronics devices has prompted execution of electronic equipment suited for electric power systems, with quick reaction contrasted with the line frequency.

The focal point of this paper on a unified power quality condition (UPQC). The UPQC is one type of the Active Power Filter (APF) where shunt and series APF functionalities are incorporated together to accomplish better control more than several power quality issues at the same time. The UPQC is controlled to regulate the real and reactive power, voltage level at Point of Common Coupling (PCC). Simulations were carried out to demonstrate the adequacy of the proposed remuneration approach. Figure 1. Shows the general block diagram of UPQC. In the current literature, aligned such that promulgation of the wind probability has been detailed section 2 followed by objective function of the projected algorithm has been discussed in section 3. The meta-heuristic model of particle swarm optimization and its application has been illustrated in section 4. At last the final section oriented towards the elucidation about the deduction of the investigation.



Fig. 1. UPQC general block diagram representation

2. Probabilistic in dissemination of wind

The power from WECS is stochastic in nature attributable to changing pace of the wind in the land territory. In this analysis, the discrete Markov analysis is utilized to estimate the varieties of twist in the area as in [24] The speed of the wind states is counted by the ramifications of discrete Markov analysis as abridged in Table 1 and probability density function supported picture as in Figure 1. Facilitate the above examined technique is fused to find the probability of the WES control as appeared in Figure 2 and specified in Table 2.

Objective Function

The intention of this investigation is to allocate the ESS optimally by PSO, to capture the surplus power produced by the WES and enhance voltage profile of the assumed IEEE 30 bus test system by way of [25] as observed in Figure 3 and a new demonstration of IEEE 57 bus system. However, the focal of the study to curtail the whole expenses of power system perhaps the proposed algorithm PSO must satisfy the enumerated constraints for the appropriate functioning power system The goal of this examination is to assign the ESS ideally by PSO, to catch the surplus power created by the WES and upgrade voltage profile of the expected IEEE 30 transport test system by method for [25] IEEE 57 bus system. Be that as it may, the central of the investigation to reduce the entire costs of power system maybe the proposed calculation PSO must fulfill the identified imperatives for the proper working power system. The scope of the functions is characterized to two objectives and is composed as follows,

Reduction in expenditure of the test systems:

The minimization of overall expenses is modeled as

$$ninR1 = \sum_{k=1}^{5} O_k T_k$$

Where the Ok is the operation cost probability at the consideration of k. The overall expenditure cost of the operation in (\$/h) through k described by , further the Ek is detailed as equation 2

$$T_k = T(P_{\theta t}) + T_w + T_{ess}$$

In the demonstration of (Pgt) is inducted generators task cost (\$/h), WES working expense is spoken to by Tw (\$/h) and *Tess* shows the cost of energy storage system (\$/h). Each term in the above articulation is advised as

The general costs of the conventional generator are expressed by

$$T(Pg_t) = \sum_{t=1}^{g} (a'_f + b'_f (Pg_t) + C'_f (Pg_t)^2)$$

Wherever a'_t, b'_t, c'_t are fuel coefficient of generator f and entire number of generators is represented by g.

$$T_w = t_w^{onc} \cdot P_w$$

As $t_w^{o,c}$ is WES functioning cost and power is produced by the wind is indicated by *Pw*.

The cost for the functioning of energy storage system as

$$T_{ess} = t_{ess}^{o.c} \cdot P_{capacity}$$

Where $t_{ess}^{o.c}$ intimating the expenses of ESS and *Pcapacity* is established capacity of ESS.

Progression of Voltage outline

The voltage profile headway of assumed test bus system is exhibited as,

$$minF2 = \sum_{x=1}^{m} \left(\frac{B - B_{exp}}{\Delta B^{max}} \right)^2$$

Where m is the whole include of transports the stepped through examination system. The normal voltage in the grid is communicated by . The maximum in change of voltage is indicated by $\Delta Bmax$, anyway needs to fulfill the power stream limitations as in [23] and to achieve the restrictions in voltages in transport and transformer taps and created reactive power as portrayed in following limits individually.

$$\begin{split} B_m &\leq B_k \leq B_M \\ T_m &\leq T_k \leq T_M \\ Q_{Gm} &\leq Q_k \leq Q_{GM} \end{split}$$

As Bk is voltages in the bus k, Tk is taps in the transformer k and Qk is hinting reactive power of the generator k.

Particle swarm optimization and implementation

The principle behind the PSO is to produce populace of swarms made out of colossal particles as of [1,2&5]. Every molecule is established to the errand of settling the advancement inconvenience by familiarize with idle arrangement in dimensional investigation bound of O inside the populace R. The best spot of the particle is restored in view of its swarm broad association.



The velocity vector is attested by $\begin{aligned} A_m^{z+1} &= A_m^z + h_m^{z+1} \\ h_m^{z+1} &= Sh_m^z + c_1 t_1 + (n_m^z - a_m^z) + c_2 t_2 (v_m^z - a_m^z) \\ n_m^z &= [a_{m1}^n, y_{m2}^n, \dots, y_{m0}^n] \\ v_m^z &= [a_{m1}^w, a_{m2}^w, \dots, a_{m0}^w] \end{aligned}$

As s is inertia weight, c_1 and c_2 are acceleration constants, t_1 and t_2 are random numbers in the bound of [0,1], n_m^z is best spot of particle m and a_m^z Swarm experience-based particle position. The efficacy of the projected method is improved by

$$S^z = S_o - \left(\frac{S_o - S_m}{S_o}\right)$$

Where S_M is introductory inertia weight and last inertia weight is S_m . The maximum cycle number is Z_o

Implementation of PSO

The proposed PSO model is affected in presumed IEEE 30 transport test system as Figure 3 and adjusted IEEE 57 transport system as aftereffect of rehashing the information in 30 transport system for the itemized examination of PSO for the optimal allocation of ESS. The vitality produced from this WES has been classified into five levels as marked in Table 2. The interest for the picked test system of IEEE depends on [23] and it has been multiplied for altered IEEE 57 bus system.

Conformation of IEEE 30 bus system

The evaluation arrangement of IEEE 30 bus system is designed with the end goal that qualification of twenty loads and five number of thermal power generators typified as G have been related to accepted framework at PV transports of 5, 8, 11 and 13. Not with standing that transport 1 bordered with warm plant as G turned as slack transport and lingering buses are locked in as PQ transport as in [25]. The WES has been consolidated to bus 2 and spoke to as W in Figure 3 with the volume of 113 MW.

Conformation of modified IEEE 57 bus system

The evaluation arrangement of IEEE 57 transport framework is designed with the end goal that privilege of forty burdens and seven number of warm power generators encapsulated as G have been related to expected framework at PV transports of 5, 8, 10, 11, 13, 16 and 22. In addition to that bus 1 adjoined with thermal plant as G turned as slack bus and residual buses are engaged as PQ bus. The WES has been combined to buses 2 and 4 represented as W in Fig 3 with the volume of 226 MW. The arranged model of PSO is actualized as takes after

Step 1: The particles of M arbitrary yielded to formulate population P, subject to satisfy all constraints.

Step 2: Initialize velocity vectors l and u for every particle.

Step 3: Discrete Markov analysis is imposed to segregate five optimal conditions.

Step 4: Enumerate the fitness value of every particle in population P.

Step 5: Verify l and u for finest position.

Step 6: Shift to step 11 or else move to next step.

Step 7: Iteration = Iteration + 1.

Step 8: Refurbish the particle position and velocity vectors l and u.

Step 9: Replicate population Q from population P and amalgamate P and Q.

Step 10: Fix the finest particles of M from population P.

Step 11: Substantiate all four scenarios and validate lowest expenditure and voltage divergence if criteria is not satisfied move to step 7.

Step 13: Allotment of ESS optimally.

Step 14: Stop.

The flowchart of the proposed algorithm is shown in Fig 1.



In this case, OPF is connected to examination test, the genuine power misfortune has been bit by bit declining when the wind power is admitted to the system continuously as in Table 7. Simultaneously, the activity cost of the examination system has been decreasing as summarized in Table 6. The voltage profile for this assumed test system is advised in Table 3.

Circuit Modelling of UPQC

The control system consists of three major elements, which are shunt inverter control, series inverter control, and DC/DC converter control. When the level of the source voltage is maintained at 1.0 p.u., the system works in normal mode. When the level falls between 0.5 and 1.0 p.u. or higher than 1.0 p.u., the system works in voltage sag or swell mode. When the level is lower than 0.5 p.u., the system works in interruption mode. In normal mode, the series inverter injects the zero voltage and the shunt inverter absorbs the current harmonics generated by the load. The DC/DC converter works in charge mode or standby mode depending on the voltage level of the super capacitors.

In voltage hang o swell mode, the arrangements inverter infuses the replaying voltage to keep up the heap voltage steady. The shunt inverter retains the present sounds produced by the heap and the DC/DC converter works in standby mode. In voltage interruption mode, the series inverter is disconnected from the line and the circuit breaker is opened to isolate the source side. The shunt inverter starts to work as an AC voltage source. The DC/DC converter works in discharge mode to supply the energy stored in the supercapacitors to the



Fig.2 30 -bus system with Wind Power Distribution for With Facts







Thirty-Bus System for Wind Power Distribution without FACTS

The Real power at bus-4 is shown in Fig4.4 and its value is 1.5*105watts. The Reactive power at bus-4 is shown in Fig. 4.5 and its value is 4.5*104 watts. The voltage of the 12-bus system is shown in Fig.4.6 and its peak value is 0.85*104V.

The real power at bus-12 is shown in Fig.4.7 and its value is 6.4*105 watts. The reactive power at bus-12 is shown in fig.4.8 and its value is 2.4*105 watts. The voltage of the 26-bus system is shown in Fig.4.9 and its peak value is 8000V.

The real power at bus-26 is shown in Fig.4.10 and its value is 2.25105 watts.

The reactive power at bus-26 is shown in Fig.4.11 and its value is 6.9*105watts.

0.5







Consequences and deliberation

In this effort, two plans have been inspected practically equivalent to evaluation framework united WES and test framework coordinate with mix of WES and ESS. The OPF (ideal power stream) technique and anticipated strategy PSO are connected over the above proclaimed cases for corresponded thought and nitty gritty as takes after.

Comparison of real and reactive power:

| Bus no | P(MW) | P(MW) | Q (MVAR) | Q (MVAR) |
|--------|---------------|------------|---------------|------------|
| | without Facts | with Facts | without Facts | With Facts |
| 4 | 0.149 | 0.163 | 0.049 | 0.051 |
| 5 | 0.138 | 0.152 | 0.091 | 0.113 |
| 6 | 0.126 | 0.149 | 0.106 | 0.118 |
| 7 | 0.123 | 0.145 | 0.103 | 0.114 |
| 8 | 0.146 | 0.161 | 0.098 | 0.104 |
| 10 | 0.153 | 0.190 | 0.099 | 0.101 |
| 11 | 0.367 | 0.360 | 0.109 | 0.113 |
| 12 | 0.356 | 0.423 | 0.108 | 0.150 |
| 13 | 0.294 | 0.356 | 0.122 | 0.138 |
| 15 | 0.286 | 0.345 | 0.128 | 0.146 |
| 16 | 0.281 | 0.338 | 0.118 | 0.136 |

| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | |
|--|----|-------|-------|-------|-------|
| 19 0.277 0.327 0.108 0.105 20 0.198 0.229 0.081 0.096 21 0.144 0.169 0.047 0.055 22 0.632 0.717 0.337 0.446 23 0.548 0.614 0.281 0.326 | 17 | 0.279 | 0.334 | 0.114 | 0.128 |
| 20 0.198 0.229 0.081 0.096 21 0.144 0.169 0.047 0.055 22 0.632 0.717 0.337 0.446 23 0.548 0.614 0.281 0.326 | 19 | 0.277 | 0.327 | 0.108 | 0.105 |
| 21 0.144 0.169 0.047 0.055 22 0.632 0.717 0.337 0.446 23 0.548 0.614 0.281 0.326 | 20 | 0.198 | 0.229 | 0.081 | 0.096 |
| 22 0.632 0.717 0.337 0.446 23 0.548 0.614 0.281 0.326 | 21 | 0.144 | 0.169 | 0.047 | 0.055 |
| 23 0.548 0.614 0.281 0.326 | 22 | 0.632 | 0.717 | 0.337 | 0.446 |
| | 23 | 0.548 | 0.614 | 0.281 | 0.326 |
| 25 0.364 0.377 1.14 1.185 | 25 | 0.364 | 0.377 | 1.14 | 1.185 |
| 26 0.218 0.257 0.685 0.807 | 26 | 0.218 | 0.257 | 0.685 | 0.807 |
| 27 0.210 0.248 0.523 0.568 | 27 | 0.210 | 0.248 | 0.523 | 0.568 |
| 28 0.221 0.263 0.256 0.276 | 28 | 0.221 | 0.263 | 0.256 | 0.276 |
| 30 0.239 0.274 0.228 0.254 | 30 | 0.239 | 0.274 | 0.228 | 0.254 |

Analysis of IEEE 30 bus system Application of OPF

In this case, OPF is applied to analysis test system, the real power loss has been gradually declining when the wind power is admitted to the system progressively as in Table 7. Simultaneously, the operation cost of the appraisal system has been decreasing as summarized in Table 6. The voltage profile for this assumed test system is briefed in Table 3. **IEEE 30 bus system integrated WES**

| WIND POWER | 0 | 14.54 | 55.79 | 98.12 | 113 |
|------------|---------|---------|---------|---------|---------|
| | (MW) | (MW) | (MW) | (MW) | (MW) |
| BUS | Voltage | Voltage | Voltage | Voltage | Voltage |
| | (p.u) | (p.u) | (p.u) | (p.u) | (p.u) |
| 1 | 1.06 | 1.06 | 1.06 | 1.06 | 1.06 |
| 2 | 1.045 | 1.045 | 1.045 | 1.045 | 1.045 |
| 3 | 1.012 | 1.012 | 1.013 | 1.014 | 1.015 |
| 4 | 1.007 | 1.008 | 1.008 | 1.009 | 1.01 |
| 5 | 1.01 | 1.01 | 1.01 | 1.01 | 1.02 |
| 6 | 1.009 | 1.009 | 1.009 | 1.009 | 1.009 |
| 7 | 1.001 | 1.001 | 1.002 | 1.002 | 1.002 |
| 8 | 1.01 | 1.01 | 1.01 | 1.01 | 1.01 |
| 9 | 1.05 | 1.05 | 1.05 | 1.05 | 1.05 |
| 10 | 1.044 | 1.044 | 1.044 | 1.044 | 1.044 |
| 11 | 1.082 | 1.082 | 1.082 | 1.082 | 1.082 |
| 12 | 1.055 | 1.056 | 1.056 | 1.057 | 1.057 |
| 13 | 1.071 | 1.071 | 1.071 | 1.072 | 1.072 |
| 14 | 1.041 | 1.041 | 1.041 | 1.041 | 1.041 |
| 15 | 1.036 | 1.036 | 1.036 | 1.037 | 1.037 |
| 16 | 1.043 | 1.043 | 1.043 | 1.043 | 1.044 |
| 17 | 1.039 | 1.039 | 1.039 | 1.039 | 1.039 |
| 18 | 1.027 | 1.027 | 1.027 | 1.027 | 1.027 |
| 19 | 1.024 | 1.024 | 1.025 | 1.025 | 1.025 |
| 20 | 1.028 | 1.028 | 1.029 | 1.029 | 1.029 |
| 21 | 1.031 | 1.032 | 1.032 | 1.032 | 1.032 |
| 22 | 1.032 | 1.032 | 1.033 | 1.033 | 1.033 |
| 23 | 1.026 | 1.026 | 1.026 | 1.026 | 1.026 |
| 24 | 1.020 | 1.02 | 1.021 | 1.021 | 1.021 |
| 25 | 1.016 | 1.016 | 1.016 | 1.017 | 1.017 |
| 26 | 0.998 | 0.998 | 0.999 | 0.999 | 0.999 |
| 27 | 1.022 | 1.022 | 1.022 | 1.023 | 1.023 |
| 28 | 1.006 | 1.006 | 1.007 | 1.008 | 1.006 |

| 29 | 1.002 | 1.002 | 1.003 | 1.004 | 1.004 |
|----|-------|-------|-------|-------|-------|
| 30 | 0.991 | 0.991 | 0.992 | 0.992 | 0.993 |

Table 3. Voltage outline for IEEE 30 bus system with WES

IEEE 30 bus system combined with WES and ESS

In this exertion, ESS has been coupled and the area for the acceptance of the ESS has been characterized by the OPF as précised in Table 4. The whole size of ESS is 43.2 MW. The

connection of ESS has occasioned to diminishing the activity cost and also genuine power loss of the test system accepted as explained in Table 7. The extent of voltage in each clean is shown in Table 4.

| | | OPF | | | | |
|-------------------|---------|-----------|-----------|-------------|----------|--|
| WIND | 0 | 14.54 | 55.79 | 98.12 | 113 | |
| POWER | (MW) | (MW) | (MW) | (MW) | (MW) | |
| BUS | Voltage | Voltage | Voltage | Voltage | Voltage | |
| | (p.u) | (p.u) | (p.u) | (p.u) | (p.u) | |
| 1 | 1.06 | 1.06 | 1.06 | 1.06 | 1.06 | |
| 2 | 1.045 | 1.045 | 1.045 | 1.045 | 1.045 | |
| 3 | 1.012 | 1.034 | 1.035 | 1.036 | 1.036 | |
| 4 | 1.007 | 1.031 | 1.032 | 1.032 | 1.032 | |
| 5 | 1.01 | 0.985 | 0.985 | 0.986 | 0.986 | |
| 6 | 1.009 | 1.032 | 1.033 | 1.033 | 1.033 | |
| 7 | 1.001 | 1.005 | 1.006 | 1.006 | 1.006 | |
| 8 | 1.01 | 1.02 | 1.021 | 1.021 | 1.021 | |
| 9 | 1.05 | 1.091 | 1.091 | 1.092 | 1.092 | |
| 10 | 1.044 | 1.11 | 1.111 | 1.111 | 1.111 | |
| 11 | 1.082 | 1.091 | 1.091 | 1.092 | 1.092 | |
| 12 | 1.055 | 1.102 | 1.103 | 1.104 | 1.104 | |
| 13 | 1.071 | 1.102 | 1.103 | 1.104 | 1.104 | |
| 14 | 1.041 | 1.098 | 1.098 | 1.099 | 1.099 | |
| 15 | 1.036 | 1.103 | 1.104 | 1.104 | 1.104 | |
| 16 | 1.043 | 1.099 | 1.099 | 1.100 | 1.100 | |
| 17 | 1.039 | 1.102 | 1.103 | 1.103 | 1.103 | |
| 18 | 1.027 | 1.133 | 1.134 | 1.134 | 1.135 | |
| 19 | 1.024 | 1.154 | 1.155 | 1.155 | 1.155 | |
| 20 | 1.028 | 1.142 | 1.143 | 1.144 | 1.144 | |
| 21 | 1.031 | 1.104 | 1.105 | 1.106 | 1.106 | |
| 22 | 1.032 | 1.107 | 1.108 | 1.108 | 1.108 | |
| 23 | 1.026 | 1.093 | 1.094 | 1.095 | 1.095 | |
| 24 | 1.02 | 1.089 | 1.089 | 1.09 | 1.09 | |
| 25 | 1.016 | 1.07 | 1.071 | 1.071 | 1.071 | |
| 26 | 0.998 | 1.053 | 1.054 | 1.055 | 1.055 | |
| 27 | 1.022 | 1.067 | 1.067 | 1.068 | 1.068 | |
| 28 | 1.006 | 1.035 | 1.036 | 1.036 | 1.036 | |
| 29 | 1.002 | 1.048 | 1.049 | 1.049 | 1.049 | |
| 30 | 0.991 | 1.037 | 1.038 | 1.038 | 1.038 | |
| Allocation of ESS | Bus 6/2 | .5MW, Bus | 19/18.2MW | , Bus 22/5. | 6MW, Bus | |
| | 28/16MW | | | | | |
| Total size of ESS | 43.2 MW | | | | | |

Table 4. Voltage outline for IEEE 30 bus system with WES allied ESS

Implementation of PSO WES allied IEEE 30 bus system

The PSO has been executed to examination system, the real power misfortune has been drastically decreased contrasted with the symmetry condition to the utilization of OPF. As of the Table 8 misfortune in real power is 12.5061 MW, while the commitment from The purposed calculation PSO actualized to consequent investigations as the wind is 113 MW in this express the working expense of the system is \$ 9498.7/hour. The voltage profile of the buses is outstanding around the estimation of 1.01 pu as revealed in Table 5

| | | | PSO | | |
|-------|---------------|---------------|---------------|---------------|---------------|
| WIND | 0 | 14.54 | 55.79 | 98.12 | 113 |
| POWER | (MW) | (MW) | (MW) | (MW) | (MW) |
| BUS | Voltage (p.u) |
| 1 | 1.06 | 1.06 | 1.06 | 1.06 | 1.06 |
| 2 | 1.045 | 1.045 | 1.045 | 1.045 | 1.045 |
| 3 | 1.0191 | 1.0198 | 1.0185 | 1.0192 | 1.0205 |
| 4 | 1.0138 | 1.0146 | 1.0142 | 1.0140 | 1.0154 |
| 5 | 1.01 | 1.01 | 1.01 | 1.01 | 1.01 |
| 6 | 1.0126 | 1.0127 | 1.0128 | 1.0133 | 1.0134 |
| 7 | 1.0036 | 1.0037 | 1.0038 | 1.0041 | 1.0041 |
| 8 | 1.01 | 1.01 | 1.01 | 1.01 | 1.01 |
| 9 | 1.0528 | 1.0529 | 1.0529 | 1.0529 | 1.0532 |
| 10 | 1.0472 | 1.0476 | 1.0477 | 1.0479 | 1.0488 |
| 11 | 1.0820 | 1.0820 | 1.0820 | 1.0820 | 1.0820 |
| 12 | 1.0605 | 1.0589 | 1.0588 | 1.0588 | 1.0588 |
| 13 | 1.0710 | 1.0710 | 1.0710 | 1.0710 | 1.0710 |
| 14 | 1.0438 | 1.0441 | 1.0441 | 1.0441 | 1.0457 |
| 15 | 1.0392 | 1.0396 | 1.0397 | 1.0399 | 1.0405 |
| 16 | 1.0459 | 1.0468 | 1.0465 | 1.0467 | 1.0473 |
| 17 | 1.0415 | 1.0422 | 1.0425 | 1.0425 | 1.0432 |
| 18 | 1.0297 | 1.0303 | 1.0304 | 1.0307 | 1.0309 |
| 19 | 1.0272 | 1.0281 | 1.0283 | 1.0287 | 1.0297 |
| 20 | 1.0313 | 1.0330 | 1.0322 | 1.0321 | 1.0330 |
| 21 | 1.0348 | 1.0352 | 1.0353 | 1.0354 | 1.0363 |
| 22 | 1.0353 | 1.0357 | 1.0358 | 1.0359 | 1.0367 |
| 23 | 1.0286 | 1.0286 | 1.0295 | 1.0295 | 1.0296 |
| 24 | 1.0229 | 1.0235 | 1.0236 | 1.0236 | 1.0240 |
| 25 | 1.0179 | 1.0182 | 1.0184 | 1.0184 | 1.0184 |
| 26 | 1.0002 | 1.0005 | 1.0007 | 1.0008 | 1.0008 |
| 27 | 1.0231 | 1.0236 | 1.0238 | 1.0238 | 1.0238 |
| 28 | 1.0087 | 1.0087 | 1.0087 | 1.0087 | 1.0093 |
| 29 | 1.0032 | 1.0038 | 1.0039 | 1.004 | 1.0041 |
| 30 | 0.9917 | 0.9923 | 0.9925 | 0.9925 | 0.9925 |

Table 5. Voltage outline for IEEE 30 bus system with WES

WES and ESS associated IEEE 30 bus system

In this specific circumstance, the PSO has been inspected over the assessed test system with the osmosis of ESS. The PSO has separated the situation of ESS with regards to the buses 7, 16 and 30 correspondingly. The whole limit of ESS associated is 29.2 MW as indicated in Table 6. In the test system, vigorous voltage diagram has been seen according to Table 8. The span of ESS joined in the midst of the execution by OPF is slighter than execution by PSO, regardless the activity cost of test framework in PSO is temperate of \$ 9512.20/hour versus \$ 9832.41/hour in OPF for the zero penetration of the WES control. In PSO if the whole intensity of WES infused to the system the costs is \$ 9498.70/hour against \$ 9509.77/hour for OPF as saw in the Tables 7 and 8 separately. Haphazardly translating the pa swarm improvement against its partner OPF for the investigation of WES, its consumption are \$ 9740.26/hour and \$ 9502.50/hour separately as inspired in Figure 4. Another investigation of same case ESS joined WES the cost is \$9758.72/ticle for OPF versus \$9502.70/hour for PSO as portrayed in Figure 5.

| PSO | | | | | |
|-------------------|---------------|-----------------|----------------|---------------|---------------|
| WIND POWER | 0 | 14.54 | 55.79 | 98.12 | 113 |
| | (MW) | (MW) | (MW) | (MW) | (MW) |
| BUS | Voltage (p.u) | Voltage (p.u) | Voltage (p.u) | Voltage (p.u) | Voltage (p.u) |
| 1 | 1.06 | 1.06 | 1.06 | 1.06 | 1.06 |
| 2 | 1.045 | 1.045 | 1.045 | 1.045 | 1.045 |
| 3 | 1.0458 | 1.0457 | 1.0457 | 1.0460 | 1.0464 |
| 4 | 1.0435 | 1.0435 | 1.0435 | 1.0438 | 1.0442 |
| 5 | 0.9928 | 0.9927 | 0.9927 | 0.9929 | 0.9931 |
| 6 | 1.0474 | 1.0471 | 1.0472 | 1.0475 | 1.0479 |
| 7 | 1.0175 | 1.0173 | 1.0173 | 1.0176 | 1.0179 |
| 8 | 1.0358 | 1.0355 | 1.0355 | 1.0359 | 1.0365 |
| 9 | 1.1084 | 1.1077 | 1.1078 | 1.1088 | 1.1089 |
| 10 | 1.1286 | 1.1276 | 1.1278 | 1.1290 | 1.1290 |
| 11 | 1.1084 | 1.1077 | 1.1078 | 1.1088 | 1.1089 |
| 12 | 1.1162 | 1.1168 | 1.1167 | 1.1165 | 1.1176 |
| 13 | 1.1162 | 1.1168 | 1.1167 | 1.1165 | 1.1176 |
| 14 | 1.1116 | 1.1125 | 1.1124 | 1.1120 | 1.1134 |
| 15 | 1.1173 | 1.1189 | 1.1186 | 1.1180 | 1.1200 |
| 16 | 1.1151 | 1.1148 | 1.1149 | 1.1155 | 1.1159 |
| 17 | 1.1195 | 1.1188 | 1.1189 | 1.1199 | 1.1201 |
| 18 | 1.1454 | 1.1502 | 1.1492 | 1.1470 | 1.1516 |
| 19 | 1.1649 | 1.1716 | 1.1701 | 1.1669 | 1.1731 |
| 20 | 1.1552 | 1.1600 | 1.1589 | 1.1569 | 1.1615 |
| 21 | 1.1269 | 1.1238 | 1.1243 | 1.1274 | 1.1258 |
| 22 | 1.1305 | 1.1267 | 1.1274 | 1.1210 | 1.1289 |
| 23 | 1.1101 | 1.1103 | 1.1102 | 1.1107 | 1.1118 |
| 24 | 1.1082 | 1.1066 | 1.1068 | 1.1086 | 1.1085 |
| 25 | 1.0870 | 1.0863 | 1.0864 | 1.0872 | 1.0885 |
| 26 | 1.0705 | 1.0697 | 1.0699 | 1.0707 | 1.0720 |
| 27 | 1.0819 | 1.0817 | 1.0818 | 1.0820 | 1.0841 |
| 28 | 1.0501 | 1.0497 | 1.0498 | 1.0502 | 1.0521 |
| 29 | 1.0633 | 1.0631 | 1.0631 | 1.0633 | 1.0654 |
| 30 | 1.0525 | 1.0523 | 1.0523 | 1.0525 | 1.0547 |
| Allocation of ESS | Bus 7/12.1 M | W, Bus 16/9.7 M | IW and Bus 30/ | 7.4 MW | |
| Capacity of ESS | 29.2 MW | | | | |

Table 6. Voltage outline for IEEE 30 bus system with WES allied ESS

| Wind | OPF | | | | | |
|---------------|-------------------------------|-----------|------------------------|-----------|--|--|
| Power (MW) | Total Real power loss (MW) | | Operation Cost (\$/hr) | | | |
| | Exclusion | Inclusion | Exclusion | Inclusion | | |
| | of ESS | of ESS | of ESS | of ESS | | |
| 0 | 27.447 | 19.966 | 9815.93 | 9832.41 | | |
| 14.54 | 25.402 | 18.356 | 9740.26 | 9758.72 | | |
| 55.79 | 20.480 | 14.433 | 9574.06 | 9758.72 | | |
| 98.12 | 16.714 | 11.970 | 9477.65 | 9521.28 | | |
| 113 | 15.685 | 11.319 | 9458.60 | 9509.77 | | |

Table 7. Total real power loss and operation cost for IEEE 30 bus system

| Wind Power | PSO | | | | | |
|---------------|-------------------------------|-----------|------------------------|-----------|--|--|
| (MW) | Total Real power loss (MW) | | Operation Cost (\$/hr) | | | |
| | Exclusion | Inclusion | Exclusion | Inclusion | | |
| | of ESS | of ESS | of ESS | of ESS | | |
| 0 | 14.530 | 12.663 | 9509.10 | 9512.20 | | |
| 14.54 | 14.514 | 12.531 | 9502.50 | 9502.70 | | |
| 55.79 | 14.503 | 12.532 | 9500.10 | 9502.50 | | |
| 98.12 | 14.498 | 12.502 | 9498.90 | 9498.80 | | |
| 113 | 14.266 | 12.506 | 9498.70 | 9498.70 | | |

Table 8. Total real power loss and operation cost for IEEE 30 bus system

5.1 Analysis of altered IEEE 57 bus system:

5.1.1 Application of OPF

The OPF applied to succeeding cases as

i.Altered IEEE 57 bus system integrated WES

In this case, OPF is applied to analysis test system, the real power loss has been gradually declining when the wind power is admitted to the system progressively as in Table 14. Simultaneously, the operation cost of the appraisal system has been decreasing as summarized in Table 13. The voltage profile for this assumed test system is briefed in Table 9.

| OPF | | | | | | |
|------|---------|---------|---------|---------|---------|--|
| WIND | 0 | 14.54 | 55.79 | 98.12 | 113 | |
| POWE | (MW) | (MW) | (MW) | (MW) | (MW) | |
| R | | | | | | |
| BUS | Voltag | Voltag | Voltag | Voltag | Voltag | |
| | e (p.u) | |
| 1 | 1.04 | 1.04 | 1.04 | 1.04 | 1.04 | |
| 2 | 1.01 | 1.01 | 1.01 | 1.01 | 1.01 | |
| 3 | 0.985 | 0.985 | 0.985 | 0.985 | 0.985 | |
| 4 | 0.981 | 0.981 | 0.981 | 0.981 | 0.981 | |
| 5 | 0.977 | 0.977 | 0.976 | 0.977 | 0.977 | |
| 6 | 0.980 | 0.980 | 0.980 | 0.981 | 0.981 | |
| 7 | 0.984 | 0.984 | 0.984 | 0.985 | 0.985 | |
| 8 | 1.005 | 1.005 | 1.005 | 1.006 | 1.006 | |
| 9 | 0.980 | 0.980 | 0.980 | 0.981 | 0.981 | |
| 10 | 0.986 | 0.986 | 0.986 | 0.986 | 0.986 | |
| 11 | 0.974 | 0.974 | 0.974 | 0.974 | 0.975 | |
| 12 | 1.015 | 1.015 | 1.015 | 1.015 | 1.016 | |
| 13 | 0.979 | 0.979 | 0.979 | 0.979 | 0.980 | |
| 14 | 0.970 | 0.970 | 0.970 | 0.970 | 0.971 | |
| 15 | 0.988 | 0.988 | 0.988 | 0.988 | 0.988 | |
| 16 | 1.013 | 1.013 | 1.013 | 1.014 | 1.014 | |
| 17 | 1.017 | 1.017 | 1.018 | 1.018 | 1.018 | |
| 18 | 1.000 | 1.000 | 1.001 | 1.002 | 1.002 | |
| 19 | 0.971 | 0.971 | 0.970 | 0.969 | 0.969 | |
| 20 | 0.965 | 0.965 | 0.964 | 0.962 | 0.962 | |
| 21 | 1.008 | 1.008 | 1.009 | 1.009 | 1.009 | |
| 22 | 1.010 | 1.010 | 1.011 | 1.011 | 1.011 | |
| 23 | 1.008 | 1.008 | 1.009 | 1.009 | 1.009 | |
| 24 | 0.999 | 0.999 | 1.000 | 1.000 | 1.000 | |
| 25 | 0.982 | 0.982 | 0.983 | 0.983 | 0.983 | |
| 26 | 0.959 | 0.959 | 0.960 | 0.960 | 0.960 | |
| 27 | 0.981 | 0.981 | 0.982 | 0.983 | 0.983 | |
| 28 | 0.996 | 0.996 | 0.997 | 0.998 | 0.998 | |
| 29 | 1.010 | 1.010 | 1.010 | 1.011 | 1.011 | |
| 30 | 0.963 | 0.963 | 0.964 | 0.965 | 0.965 | |
| 31 | 0.936 | 0.936 | 0.937 | 0.937 | 0.937 | |
| 32 | 0.950 | 0.950 | 0.951 | 0.952 | 0.952 | |
| 33 | 0.947 | 0.948 | 0.949 | 0.949 | 0.949 | |
| 34 | 0.959 | 0.959 | 0.959 | 0.959 | 0.959 | |
| 35 | 0.966 | 0.966 | 0.967 | 0.968 | 0.968 | |
| 36 | 0.976 | 0.976 | 0.977 | 0.978 | 0.978 | |
| 37 | 0.985 | 0.985 | 0.985 | 0.986 | 0.986 | |
| 38 | 1.013 | 1.013 | 1.014 | 1.015 | 1.015 | |
| 39 | 0.983 | 0.983 | 0.984 | 0.985 | 0.985 | |
| 40 | 0.973 | 0.973 | 0.974 | 0.974 | 0.974 | |
| 41 | 0.996 | 0.996 | 0.996 | 0.997 | 0.997 | |
| 42 | 0.967 | 0.967 | 0.968 | 0.968 | 0.968 | |
| 43 | 1.010 | 1.010 | 1.02 | 1.02 | 1.02 | |

| 44 | 1.017 | 1.017 | 1.018 | 1.018 | 1.018 |
|----|-------|-------|-------|-------|-------|
| 45 | 1.036 | 1.036 | 1.036 | 1.037 | 1.037 |
| 46 | 1.060 | 1.060 | 1.061 | 1.061 | 1.061 |
| 47 | 1.033 | 1.033 | 1.034 | 1.034 | 1.034 |
| 48 | 1.027 | 1.027 | 1.028 | 1.028 | 1.028 |
| 49 | 1.036 | 1.036 | 1.036 | 1.037 | 1.037 |
| 50 | 1.024 | 1.023 | 1.024 | 1.024 | 1.024 |
| 51 | 1.053 | 1.052 | 1.053 | 1.053 | 1.053 |
| 52 | 0.980 | 0.980 | 0.981 | 0.982 | 0.982 |
| 53 | 0.971 | 0.971 | 0.972 | 0.973 | 0.973 |
| 54 | 0.996 | 0.996 | 0.997 | 0.998 | 0.998 |
| 55 | 1.031 | 1.031 | 1.032 | 1.032 | 1.032 |
| 56 | 0.968 | 0.968 | 0.969 | 0.969 | 0.969 |
| 57 | 0.965 | 0.965 | 0.965 | 0.965 | 0.965 |

Table 9. Voltage outline for altered IEEE 57 bus system with WES

Altered IEEE 57 bus system integrated combined with WES and ESS

In this effort, ESS has been coupled and the location for the induction of the ESS has been defined by the OPF as précised in Table 10. The entire magnitude of ESS is 86.4 MW. The attachment of ESS has occasioned to lessening the operation cost as well as real power loss of the test system assumed as elaborated in Table 13. The magnitude of voltage in each bus is indicated in Table 10.

| OPF | | | | | | |
|-------|---------|---------|---------|---------|---------|--|
| WIND | 0 | 14.54 | 55.79 | 98.12 | 113 | |
| POWER | (MW) | (MW) | (MW) | (MW) | (MW) | |
| BUS | Voltag | Voltag | Voltag | Voltag | Voltag | |
| | e (p.u) | |
| 1 | 1.009 | 1.011 | 1.009 | 1.01 | 1.01 | |
| 2 | 1.010 | 1.012 | 1.010 | 1.012 | 1.011 | |
| 3 | 1.002 | 1.000 | 1.003 | 1.007 | 1.009 | |
| 4 | 1.006 | 1.005 | 1.007 | 1.009 | 1.010 | |
| 5 | 1.016 | 1.017 | 1.016 | 1.015 | 1.015 | |
| 6 | 1.026 | 1.028 | 1.026 | 1.024 | 1.023 | |
| 7 | 1.025 | 1.026 | 1.025 | 1.022 | 1.021 | |
| 8 | 1.045 | 1.045 | 1.044 | 1.041 | 1.040 | |
| 9 | 1.005 | 1.005 | 1.004 | 1.002 | 1.002 | |
| 10 | 0.985 | 0.985 | 0.984 | 0.983 | 0.983 | |
| 11 | 0.984 | 0.985 | 0.984 | 0.983 | 0.983 | |
| 12 | 0.992 | 0.993 | 0.992 | 0.991 | 0.990 | |
| 13 | 0.978 | 0.978 | 0.978 | 0.977 | 0.977 | |
| 14 | 0.970 | 0.970 | 0.970 | 0.970 | 0.970 | |
| 15 | 0.988 | 0.988 | 0.988 | 0.989 | 0.989 | |
| 16 | 0.991 | 0.992 | 0.991 | 0.990 | 0.990 | |

| 17 | 0.993 | 0.994 | 0.993 | 0.992 | 0.992 |
|----------|---------|------------|------------|-----------|-------|
| 18 | 1.026 | 1.024 | 1.026 | 1.029 | 1.030 |
| 19 | 0.988 | 0.988 | 0.988 | 0.989 | 0.990 |
| 20 | 0.977 | 0.977 | 0.977 | 0.977 | 0.977 |
| 21 | 1.015 | 1.015 | 1.015 | 1.015 | 1.015 |
| 22 | 1.015 | 1.015 | 1.015 | 1.015 | 1.015 |
| 23 | 1.014 | 1.014 | 1.014 | 1.014 | 1.014 |
| 24 | 1.017 | 1.018 | 1.017 | 1.016 | 1.016 |
| 25 | 1.001 | 1.001 | 1.001 | 1.000 | 1.000 |
| 26 | 0.976 | 0.977 | 0.976 | 0.975 | 0.975 |
| 27 | 1.013 | 1.014 | 1.013 | 1.011 | 1.011 |
| 28 | 1.034 | 1.035 | 1.003 | 1.031 | 1.031 |
| 29 | 1.051 | 1.052 | 1.050 | 1.048 | 1.047 |
| 30 | 0.980 | 0.981 | 0.980 | 0.979 | 0.979 |
| 31 | 0.951 | 0.951 | 0.951 | 0.950 | 0.950 |
| 32 | 0.960 | 0.960 | 0.960 | 0.960 | 0.959 |
| 33 | 0.958 | 0.958 | 0.958 | 0.957 | 0.957 |
| 34 | 0.967 | 0.967 | 0.967 | 0.966 | 0.966 |
| 35 | 0.973 | 0.973 | 0.973 | 0.973 | 0.973 |
| 36 | 0.982 | 0.983 | 0.982 | 0.982 | 0.982 |
| 37 | 0.991 | 0.991 | 0.991 | 0.990 | 0.990 |
| 38 | 1.016 | 1.016 | 1.016 | 1.016 | 1.016 |
| 39 | 0.989 | 0.989 | 0.989 | 0.988 | 0.988 |
| 40 | 0.980 | 0.980 | 0.980 | 0.979 | 0.979 |
| 41 | 1.007 | 1.007 | 1.007 | 1.006 | 1.005 |
| 42 | 0.975 | 0.975 | 0.975 | 0.974 | 0.974 |
| 43 | 1.020 | 1.021 | 1.020 | 1.019 | 1.018 |
| 44 | 1.019 | 1.019 | 1.019 | 1.019 | 1.019 |
| 45 | 1.035 | 1.034 | 1.035 | 1.036 | 1.036 |
| 46 | 1.060 | 1.060 | 1.060 | 1.060 | 1.060 |
| 4/ | 1.034 | 1.034 | 1.034 | 1.034 | 1.034 |
| 48 | 1.029 | 1.029 | 1.029 | 1.029 | 1.029 |
| 49 | 1.038 | 1.038 | 1.038 | 1.037 | 1.037 |
| 50 | 1.024 | 1.025 | 1.024 | 1.023 | 1.025 |
| 52 | 1.032 | 1.033 | 1.032 | 1.030 | 1.030 |
| 53 | 1.020 | 1.021 | 1.017 | 1.017 | 1.010 |
| 54 | 1.01 | 1.011 | 1.009 | 1.007 | 1.000 |
| 55 | 1.03 | 1.051 | 1.029 | 1.027 | 1.020 |
| 56 | 0.975 | 0.975 | 0.975 | 0.974 | 0.974 |
| 57 | 0.970 | 0.970 | 0.971 | 0.970 | 0.969 |
| Allocati | Bus 6/5 | MW. Bus | s 8/36.4 N | IW. Bus 9 | /11.2 |
| on of | MW. Bi | 1s12 /32 N | лW | , 200) | |
| ESS | | | | | |
| Total | 86.4 MW | | | | |
| size of | | | | | |
| ESS | | | | | |

Table 10. Voltage outline for altered IEEE 57 bus system with WES allied ESS

Implementation of PSO

The purposed algorithm PSO implemented to subsequent studies as

WES allied modified IEEE 57 bus system

The PSO has been implemented to inspection system, the real power loss has been dramatically reduced compared to the symmetry circumstance to the application of OPF. As of the Table 14 loss in real power is 11.848 MW, while the contribution from the wind is 226 MW in this state the functioning cost of the system is \$ 19007.4/ hour. The voltage profile of the buses is admirable around the value of 1.01 pu as disclosed in Table 11.

| PSO | | | | | | |
|------|---------|---------|---------|---------|---------|--|
| WIND | 0 | 14.54 | 55.79 | 98.12 | 113 | |
| POWE | (MW) | (MW) | (MW) | (MW) | (MW) | |
| R | | | | | | |
| BUS | Voltag | Voltag | Voltag | Voltag | Voltag | |
| | e (p.u) | |
| 1 | 1.0400 | 1.0400 | 1.0400 | 1.0400 | 1.0400 | |
| 2 | 1.0100 | 1.0100 | 1.0100 | 1.0100 | 1.0100 | |
| 3 | 0.9850 | 0.9850 | 0.9850 | 0.9850 | 0.9850 | |
| 4 | 0.9867 | 0.9772 | 0.9777 | 0.9774 | 0.9775 | |
| 5 | 0.9759 | 0.9728 | 0.9732 | 0.9729 | 0.9730 | |
| 6 | 0.9800 | 0.9800 | 0.9800 | 0.9800 | 0.9800 | |
| 7 | 0.9567 | 0.9808 | 0.9810 | 0.9809 | 0.9809 | |
| 8 | 0.9587 | 1.0050 | 1.0050 | 1.0050 | 1.0050 | |
| 9 | 0.9800 | 0.9800 | 0.9800 | 0.9800 | 0.9800 | |
| 10 | 0.9822 | 0.9806 | 0.9809 | 0.9809 | 0.9809 | |
| 11 | 0.9678 | 0.9655 | 0.9660 | 0.9660 | 0.9659 | |
| 12 | 1.0150 | 1.0150 | 1.0150 | 1.0150 | 1.0150 | |
| 13 | 0.9712 | 0.9678 | 0.9685 | 0.9684 | 0.9684 | |
| 14 | 0.9611 | 0.9561 | 0.9569 | 0.9569 | 0.9568 | |
| 15 | 0.9770 | 0.9736 | 0.9744 | 0.9744 | 0.9743 | |
| 16 | 0.9964 | 0.9961 | 0.9968 | 0.9968 | 0.9967 | |
| 17 | 0.9979 | 0.9975 | 0.9984 | 0.9983 | 0.9983 | |
| 18 | 1.0762 | 0.9951 | 0.9957 | 0.9953 | 0.9955 | |
| 19 | 1.2998 | 0.9632 | 0.9638 | 0.9636 | 0.9636 | |
| 20 | 1.1776 | 0.9558 | 0.9564 | 0.9564 | 0.9563 | |
| 21 | 1.0500 | 0.9940 | 0.9950 | 0.9948 | 0.9948 | |
| 22 | 1.0206 | 0.9950 | 0.9960 | 0.9958 | 0.9958 | |
| 23 | 1.0180 | 0.9932 | 0.9942 | 0.9940 | 0.9940 | |
| 24 | 0.9905 | 0.9804 | 0.9817 | 0.9812 | 0.9813 | |
| 25 | 0.9711 | 0.9584 | 0.9599 | 0.9593 | 0.9594 | |
| 26 | 0.9542 | 0.9471 | 0.9480 | 0.9476 | 0.9477 | |
| 27 | 0.9591 | 0.9692 | 0.9701 | 0.9696 | 0.9697 | |
| 28 | 0.9680 | 0.9845 | 0.9852 | 0.9848 | 0.9849 | |

| 29 | 0.9767 | 0.9973 | 0.9980 | 0.9975 | 0.9976 |
|----|--------|--------|--------|--------|--------|
| 30 | 0.9528 | 0.9392 | 0.9407 | 0.9401 | 0.9403 |
| 31 | 0.9299 | 0.9145 | 0.9159 | 0.9155 | 0.9155 |
| 32 | 0.9506 | 0.9334 | 0.9346 | 0.9343 | 0.9343 |
| 33 | 0.9483 | 0.9311 | 0.9322 | 0.9320 | 0.9320 |
| 34 | 0.9576 | 0.9395 | 0.9407 | 0.9404 | 0.9404 |
| 35 | 0.9656 | 0.9475 | 0.9486 | 0.9484 | 0.9484 |
| 36 | 0.9761 | 0.9580 | 0.9591 | 0.9589 | 0.9589 |
| 37 | 0.9864 | 0.9681 | 0.9691 | 0.9690 | 0.9689 |
| 38 | 1.0185 | 0.9989 | 0.9999 | 0.9997 | 0.9997 |
| 39 | 0.9840 | 0.9658 | 0.9669 | 0.9667 | 0.9667 |
| 40 | 0.9723 | 0.9546 | 0.9557 | 0.9555 | 0.9555 |
| 41 | 0.9891 | 0.9828 | 0.9836 | 0.9836 | 0.9835 |
| 42 | 0.9640 | 0.9552 | 0.9559 | 0.9558 | 0.9558 |
| 43 | 1.0031 | 0.9996 | 1.0002 | 1.0002 | 1.0001 |
| 44 | 1.0195 | 1.0033 | 1.0042 | 1.0041 | 1.0041 |
| 45 | 1.0352 | 1.0263 | 1.0270 | 1.0269 | 1.0269 |
| 46 | 1.0567 | 1.0473 | 1.0480 | 1.0480 | 1.0479 |
| 47 | 1.0349 | 1.0213 | 1.0221 | 1.0220 | 1.0220 |
| 48 | 1.0297 | 1.0145 | 1.0154 | 1.0153 | 1.0153 |
| 49 | 1.0354 | 1.0238 | 1.0246 | 1.0246 | 1.0245 |
| 50 | 1.0203 | 1.0117 | 1.0124 | 1.0124 | 1.0123 |
| 51 | 1.0457 | 1.0427 | 1.0433 | 1.0433 | 1.0432 |
| 52 | 0.9541 | 0.9708 | 0.9713 | 0.9710 | 0.9711 |
| 53 | 0.9484 | 0.9630 | 0.9635 | 0.9632 | 0.9633 |
| 54 | 0.9850 | 0.9935 | 0.9936 | 0.9936 | 0.9936 |
| 55 | 1.0306 | 1.0331 | 1.0330 | 1.0333 | 1.0331 |
| 56 | 0.9705 | 0.9593 | 0.9600 | 0.9599 | 0.9599 |
| 57 | 0.9694 | 0.9566 | 0.9573 | 0.9571 | 0.9572 |

Table 11. Voltage outline for altered IEEE 57 bus system with WES

WES and ESS associated in altered IEEE 57 bus system

In this context, the PSO has been examined over the estimated test system with the assimilation of ESS. The PSO has demarcated the position of ESS as to the buses 6, 8, 9 and 12 correspondingly. The entire capacity of ESS connected is 43.2 MW as specified in Table 12. In the test system, robust voltage outline has been observed as per Table 14. The size of ESS attached amid the execution by OPF is slighter than performance by PSO, nonetheless the operation cost of test system in PSO is economical of \$ 19202.40/hour versus \$ 19631.86/hour in OPF for the zero infiltration of the WES power. In PSO if the entire power of WES injected to the system expenses is \$ 19005.00/hour against \$ the 19117.20/hour for OPF as observed in the Tables 13 and 14 respectively.

| PSO | | | | | | |
|------------|---------------|---------------|---------------|---------------|---------------|--|
| WIND POWER | 0 | 14.54 | 55.79 | 98.12 | 113 | |
| | (MW) | (MW) | (MW) | (MW) | (MW) | |
| BUS | Voltage (p.u) | |
| 1 | 1.0400 | 1.0400 | 1.0400 | 1.0400 | 1.0400 | |
| 2 | 1.0100 | 1.0100 | 1.0100 | 1.0100 | 1.0100 | |
| 3 | 0.9850 | 0.9850 | 0.9850 | 0.9850 | 0.9850 | |
| 4 | 0.9777 | 0.9783 | 0.9781 | 0.9778 | 0.9778 | |
| 5 | 0.9732 | 0.9738 | 0.9736 | 0.9734 | 0.9733 | |
| 6 | 0.9800 | 0.9800 | 0.9800 | 0.9800 | 0.9800 | |
| 7 | 0.9812 | 0.9813 | 0.9810 | 0.9811 | 0.9812 | |
| 8 | 1.0050 | 1.0050 | 1.0050 | 1.0050 | 1.0050 | |
| 9 | 0.9800 | 0.9800 | 0.9800 | 0.9800 | 0.9800 | |
| 10 | 0.9811 | 0.9813 | 0.9810 | 0.9809 | 0.9812 | |
| 11 | 0.9664 | 0.9667 | 0.9663 | 0.9662 | 0.9665 | |
| 12 | 1.0150 | 1.0150 | 1.0150 | 1.0150 | 1.0150 | |
| 13 | 0.9691 | 0.9695 | 0.9690 | 0.9688 | 0.9692 | |
| 14 | 0.9578 | 0.9582 | 0.9577 | 0.9573 | 0.9579 | |
| 15 | 0.9753 | 0.9755 | 0.9753 | 0.9747 | 0.9754 | |
| 16 | 0.9983 | 0.9985 | 0.9982 | 0.9977 | 0.9983 | |
| 17 | 1.0000 | 1.0003 | 1.0000 | 0.9993 | 1.0001 | |
| 18 | 0.9957 | 0.9963 | 0.9962 | 0.9957 | 0.9958 | |
| 19 | 0.9645 | 0.9651 | 0.9644 | 0.9644 | 0.9645 | |
| 20 | 0.9575 | 0.9582 | 0.9571 | 0.9573 | 0.9576 | |
| 21 | 0.9957 | 0.9962 | 0.9958 | 0.9952 | 0.9958 | |
| 22 | 0.9969 | 0.9974 | 0.9968 | 0.9963 | 0.9969 | |
| 23 | 0.9951 | 0.9956 | 0.9950 | 0.9945 | 0.9951 | |
| 24 | 0.9825 | 0.9832 | 0.9825 | 0.9819 | 0.9826 | |
| 25 | 0.9608 | 0.9617 | 0.9609 | 0.9602 | 0.9609 | |
| 26 | 0.9487 | 0.9492 | 0.9487 | 0.9482 | 0.9488 | |
| 27 | 0.9704 | 0.9710 | 0.9705 | 0.9701 | 0.9705 | |
| 28 | 0.9855 | 0.9860 | 0.9856 | 0.9853 | 0.9856 | |
| 29 | 0.9982 | 0.9986 | 0.9983 | 0.9980 | 0.9983 | |
| 30 | 0.9416 | 0.9426 | 0.9417 | 0.9410 | 0.9418 | |
| 31 | 0.9169 | 0.9177 | 0.9169 | 0.9162 | 0.9170 | |
| 32 | 0.9355 | 0.9362 | 0.9355 | 0.9350 | 0.9357 | |
| 33 | 0.9332 | 0.9338 | 0.9331 | 0.9326 | 0.9333 | |
| 34 | 0.9417 | 0.9423 | 0.9416 | 0.9411 | 0.9418 | |
| 35 | 0.9496 | 0.9502 | 0.9495 | 0.9490 | 0.9497 | |
| 36 | 0.9600 | 0.9606 | 0.9599 | 0.9595 | 0.9601 | |
| 37 | 0.9701 | 0.9706 | 0.9700 | 0.9695 | 0.9702 | |
| 38 | 1.0007 | 1.0012 | 1.0006 | 1.0002 | 1.0008 | |
| 39 | 0.9678 | 0.9684 | 0.9677 | 0.9673 | 0.9679 | |
| 40 | 0.9567 | 0.9573 | 0.9566 | 0.9561 | 0.9568 | |
| 41 | 0.9843 | 0.9848 | 0.9842 | 0.9839 | 0.9844 | |
| 42 | 0.9566 | 0.9570 | 0.9565 | 0.9562 | 0.9566 | |
| 43 | 1.0007 | 1.0011 | 1.0006 | 1.0004 | 1.0008 | |
| 44 | 1.0051 | 1.0055 | 1.0050 | 1.0045 | 1.0051 | |
| 45 | 1.0277 | 1.0279 | 1.0277 | 1.0272 | 1.0278 | |

| Total size of ESS | 58.4 MW | | | | |
|-------------------|---|--------|--------|--------|--------|
| Allocation of ESS | Bus 7/24.2 MW, Bus 22/19.4 MW, and Bus 47/14.8 MW | | | | |
| 57 | 0.9579 | 0.9582 | 0.9579 | 0.9575 | 0.9579 |
| 56 | 0.9606 | 0.9609 | 0.9606 | 0.9602 | 0.9606 |
| 55 | 1.0332 | 1.0331 | 1.0329 | 1.0331 | 1.0331 |
| 54 | 0.9938 | 0.9939 | 0.9937 | 0.9937 | 0.9938 |
| 53 | 0.9636 | 0.9639 | 0.9636 | 0.9635 | 0.9637 |
| 52 | 0.9715 | 0.9719 | 0.9716 | 0.9714 | 0.9716 |
| 51 | 1.0438 | 1.0442 | 1.0437 | 1.0436 | 1.0439 |
| 50 | 1.0133 | 1.0137 | 1.0131 | 1.0129 | 1.0133 |
| 49 | 1.0255 | 1.0260 | 1.0254 | 1.0251 | 1.0256 |
| 48 | 1.0163 | 1.0167 | 1.0162 | 1.0158 | 1.0163 |
| 47 | 1.0230 | 1.0233 | 1.0229 | 1.0225 | 1.0231 |
| 46 | 1.0490 | 1.0493 | 1.0488 | 1.0485 | 1.0490 |

Table 12. Voltage outline for altered IEEE 57 bus system with WES allied ESS

| Wind | OPF | | | |
|------------|--|--------|------------------------|------------------|
| Power (MW) | Total Real power loss (MW) Exclusion of ESS Inclusion of ESS | | Operation Cost (\$/hr) | |
| | | | Exclusion of ESS | Inclusion of ESS |
| 0 | 28.602 | 16.886 | 18831.86 | 19631.86 |
| 29.08 | 27.638 | 17.801 | 18678.52 | 19480.52 |
| 111.58 | 25.441 | 16.652 | 18636.12 | 19348.12 |
| 196.24 | 23.996 | 16.027 | 18579.30 | 19155.30 |
| 226 | 23.679 | 15.923 | 18421.20 | 19117.20 |

Table 13. Total real power loss and operation cost for altered IEEE 57 bus system

| Wind Power (MW) | PSO | | | | |
|-----------------|-----------------------|------------------|------------------------|------------------|--|
| | Total Real power loss | (MW) | Operation Cost (\$/hr) | | |
| | Exclusion of ESS | Inclusion of ESS | Exclusion of ESS | Inclusion of ESS | |
| 0 | 12.512 | 11.231 | 19005.40 | 19202.40 | |
| 29.08 | 12.300 | 11.010 | 19035.20 | 19053.60 | |
| 111.58 | 11.726 | 11.178 | 18997.40 | 19007.40 | |
| 196.24 | 11.880 | 11.590 | 19017.40 | 19057.60 | |
| 226 | 11.848 | 11.181 | 19007.4 | 19005.00 | |

Table 14. Total real power loss and operation cost for altered IEEE 57 bus system



Fig 4: Correlation of expenses incurred by WES for 14.54 MW in the domain of OPF and PSO for IEEE 30 bus system



Fig 5: Correlation of expenses incurred by WES allied ESS for 14.54 MW in the domain of OPF and PSO for IEEE 30 bus system







Fig 6: Correlation of expenses incurred by WECS allied ESS for 55.79 MW in the domain of OPF and PS



Fig 7: Correlation of expenses incurred by WECS allied ESS for 98.12 MW in the domain of OPF and PSO



Fig 8: Correlation of expenses incurred by WECS allied ESS for 113 MW in the domain of OPF and PSO







(4, 9525 9520 9520 9515 9510 9510 9495 L 0 80 100 120 Iteration Number

Fig 10: Correlation of expenses incurred by WES for 55.79 MW in the domain of OPF and PSO for IEEE 57 bus system.

Fig 9: Correlation of expenses incurred by WES for 14.54 MW in the domain of OPF and PSO for IEEE 57 bus system.





Fig 11: Correlation of expenses incurred by WES for 98.12 MW in the domain of OPF and PSO for IEEE 57 bus system.





Fig 12: Correlation of expenses incurred by WES for 113 MW in the domain of OPF and PSO for IEEE 57 bus system.

CONCLUSION:

The effects of the coordination of wind power and Energy Storage Systems in three cases are examined and manifest with exhibit the adequacy of the proposed PSO strategy.

Case 1: A regular probabilistic load flow analysis for the system consider the entire wind power distribution, but without ESS installation.

Case 2: An optimal load flow (OPF) analysis to determine the best ESS allocation under the worst case scenario assuming zero wind power.

Case 3: A PSO analysis for the system consider the entire wind power distribution, but without ESS installation.

Case 4: PSO with ESS considering the entire wind distribution.

The parameters and conditions take after the information sheet in [20]. Six scenarios of wind power glean from Discrete Markov Analysis (DMA) are contemplated in these three contextual Analyses.

Case 1: The resultant bus voltages, operation cost, and losses of Case 1 are listed in Table 3. The highlighted rows represent the voltage of each generator.

It very well may be seen from Table 3 that the system operation cost and power misfortune lessens with the expansion of wind power. The total operation cost varies from 9815.93 \$/hr to 9458.6 \$/hr according to the changes of wind power from 0 to 113 MW.

Further, the system encounters both low-voltage and high voltage issues. At the point when the wind power is less than 55.79MW, the voltage at the wind generator bus practices a low-voltage issue. For particular, the voltage drops when the wind power is 0 MW. Under this circumstance, regardless of whether the voltages at the generator transports 11 and 13 are increased to 1.082 and 1.071 p.u. respectively, the low voltages still appear at buses 5, 8, 26 and 30.

Case 2: It can be seen from Table 4 that the system operation cost and power loss reduce with the increase of wind power. The Optimal Power Flow (OPF) analysis used to determine the real power loss and total cost. The total operation cost varies from 9832.1 \$/hr to 9509.5 \$/hr according to the changes of wind power from 0 to 113 MW. In this case, OPF is applied to analysis test system, the real power loss has been gradually declining when the wind power is admitted to the system progressively as in Table 7. Simultaneously, the operation cost of the appraisal system has been decreasing as summarized in Table 6. The voltage profile for this assumed test system is briefed in Table 4.

The UPQC implemented in Thirty-bus system has been successfully executed, modeled and simulated using MATLAB. The comparison of results of the thirty-bus system with and without UPQC is presented. The resemblance revealed that the real power losses are reduced by 6% by introducing the UPQC in the multibus system. The comparison of results of the thirty-bus system with & without UPQC indicates that the voltage stability is improved in the interconnected mode with UPQC.

The benefits of UPQC are sag mitigation, reduction of heat in the alternator & improvement of the voltage at load buses. The disadvantage of UPQC is that it requires a DC source to charge the DC link capacitor & the firing circuits have to be designed to operate at different frequencies.

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